



Centro Italiano Ricerche Aerospaziali



Centro Italiano Ricerche Aerospaziali

Seminari Interdisciplinari di
Cultura Aeronautica
Il Serie, I Ciclo
4° incontro

15 dicembre 2018
NELLO SPAZIO, INFINE

Il programma SPACE RIDER: le protezioni
termiche parlano italiano



- ┌ Il CIRA e la Sperimentazione «Spaziale»
 - ┌ Plasma Wind Tunnel
 - ┌ Space Qualification Labs

- ┌ L'heritage nel settore del Rientro
 - ┌ USV
 - ┌ IXV
 - ┌ Space Rider

- ┌ Le Protezioni Termiche di Space Rider : un'avventura italiana
 - ┌ CMC flap
 - ┌ La Caratterizzazione in PWT

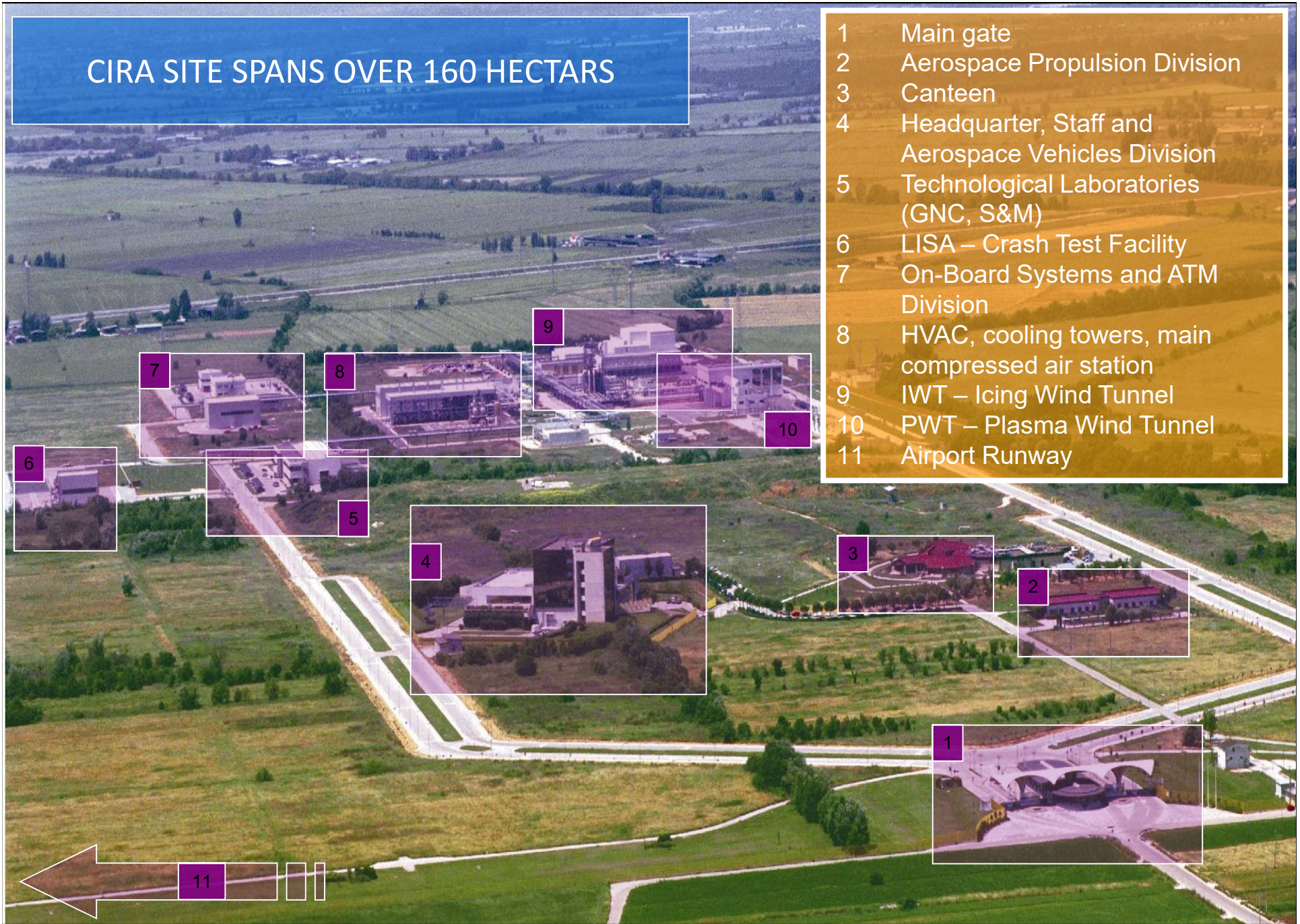


- A non-profit public-private partnership among:
 - ASI (Italian Space Agency) - 47%
 - CNR (National Council for Research) - 5%
 - Campania Region - 16%
 - Italian Aerospace Industries - 32%
- In 1989, the Italian Government entrusted CIRA of the Italian Aerospace Research Program (PRORA) management:
 - development and operation of strategic testing facilities,
 - development of strategic research programs,
 - enhancement of scientific competences and expertise.
- 370 employees and approx. 50 university students and PhD candidates a year
- Partner of the main European research programs in the aviation and space fields



CIRA SITE SPANS OVER 160 HECTARS

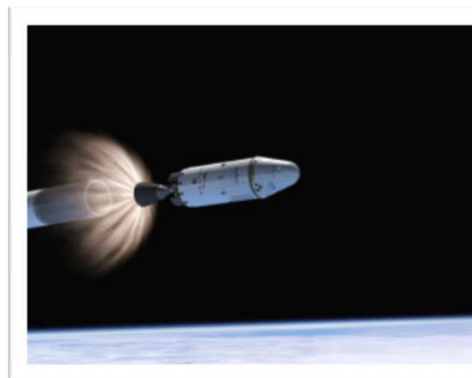
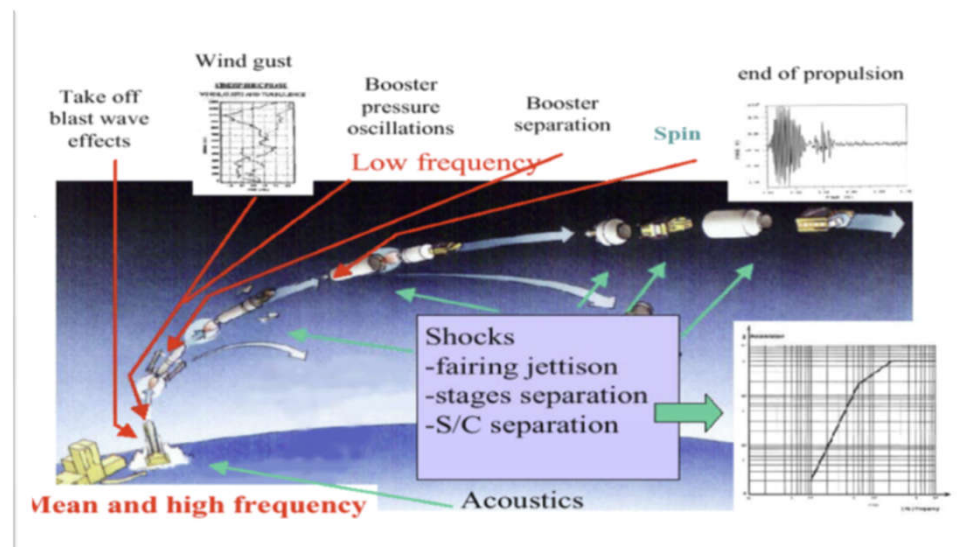
- 1 Main gate
- 2 Aerospace Propulsion Division
- 3 Canteen
- 4 Headquarter, Staff and Aerospace Vehicles Division
- 5 Technological Laboratories (GNC, S&M)
- 6 LISA – Crash Test Facility
- 7 On-Board Systems and ATM Division
- 8 HVAC, cooling towers, main compressed air station
- 9 IWT – Icing Wind Tunnel
- 10 PWT – Plasma Wind Tunnel
- 11 Airport Runway



Spacecraft structures and internal equipment are exposed to a variety of mechanical, thermal, and electromagnetic loads.

The environments, relevant to both Earth and space missions, are :

- Radiation
- **Vibration**
- **Thermal**
- Electromagnetic



One of the challenges in space qualification is to reproduce the operational environment such that critical components are tested to the limits of a mission without requiring expensive overdesign.



Steam Supply System (96,6 ton/h)



Electrical Energy Supply System (90MVA)

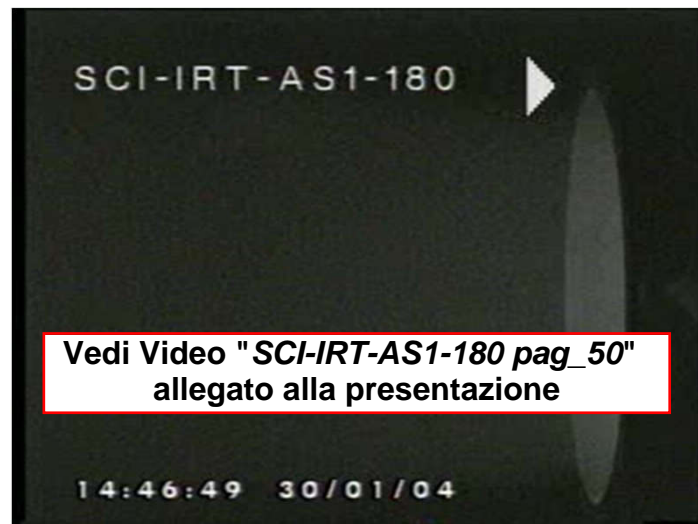


Tower Water Supply System (11700 m³/h)

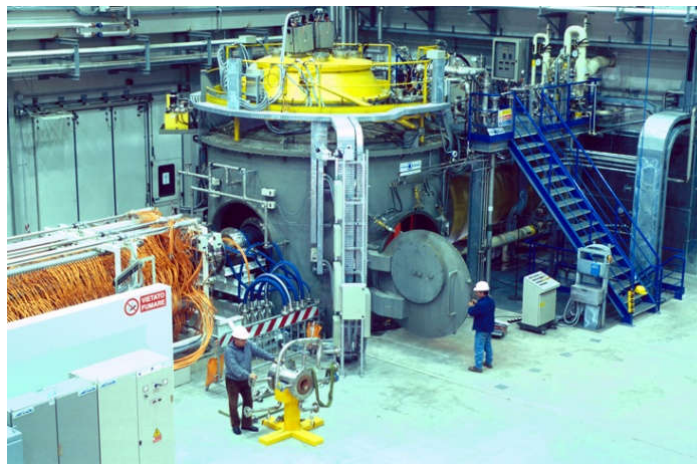


Compressed Air Supply System (3,5kg/s)

PWT – PLASMA WIND TUNNEL SCIROCCO



- GOAL: IMPROVE SAFETY OF RE-ENTRY SPACE VEHICLES
- USE: DESIGN AND TEST THERMAL PROTECTION SYSTEMS FOR SPACE VEHICLES
- OPERATIVE SINCE: 2002
- TESTING FLUID: AIR
- MAX SPEED: MACH 16
- STAGNATION TEMPERATURE: $\sim 10.000^{\circ} \text{C}$
- MAX TEST DURATIONS: < 25 MINUTES
- NOZZLE EXIT DIAMETER: 2.0 M
- NOMINAL DIMENSION OF TEST SPECIMEN: 0.6 M
- MAX POWER OF ARC HEATER: 70 MW



GHIBLI – SMALL PLASMA WIND TUNNEL SCIROCCO

- GOAL: IMPROVE SAFETY OF RE-ENTRY SPACE VEHICLES
- USE: DESIGN AND TEST SMALL SPECIMENS OF MATERIALS TO BE USED FOR THERMAL PROTECTION SYSTEMS OF SPACE VEHICLES
- TESTING FLUID: AIR, (CO₂ IS UNDER DEVELOPMENT)
- MAX SPEED: MACH 12
- STAGNATION TEMPERATURE: $\cong 10000^{\circ} \text{C}$
- MAX TEST DURATIONS: < 25 MINUTES
- NOZZLE EXIT DIAMETER : 150 MM
- NOMINAL DIMENSION OF TEST SPECIMEN: 80 MM
- MAX POWER OF ARC HEATER: 2 MW



Lab. Qualifica Spaziale

Lab. Materiali Avanzati



Lab. GN&C



Lab. Vibrazioni/Acustica



Unmanned Space Vehicle



Lab. Impatto al Suolo



Icing Wind Tunnel

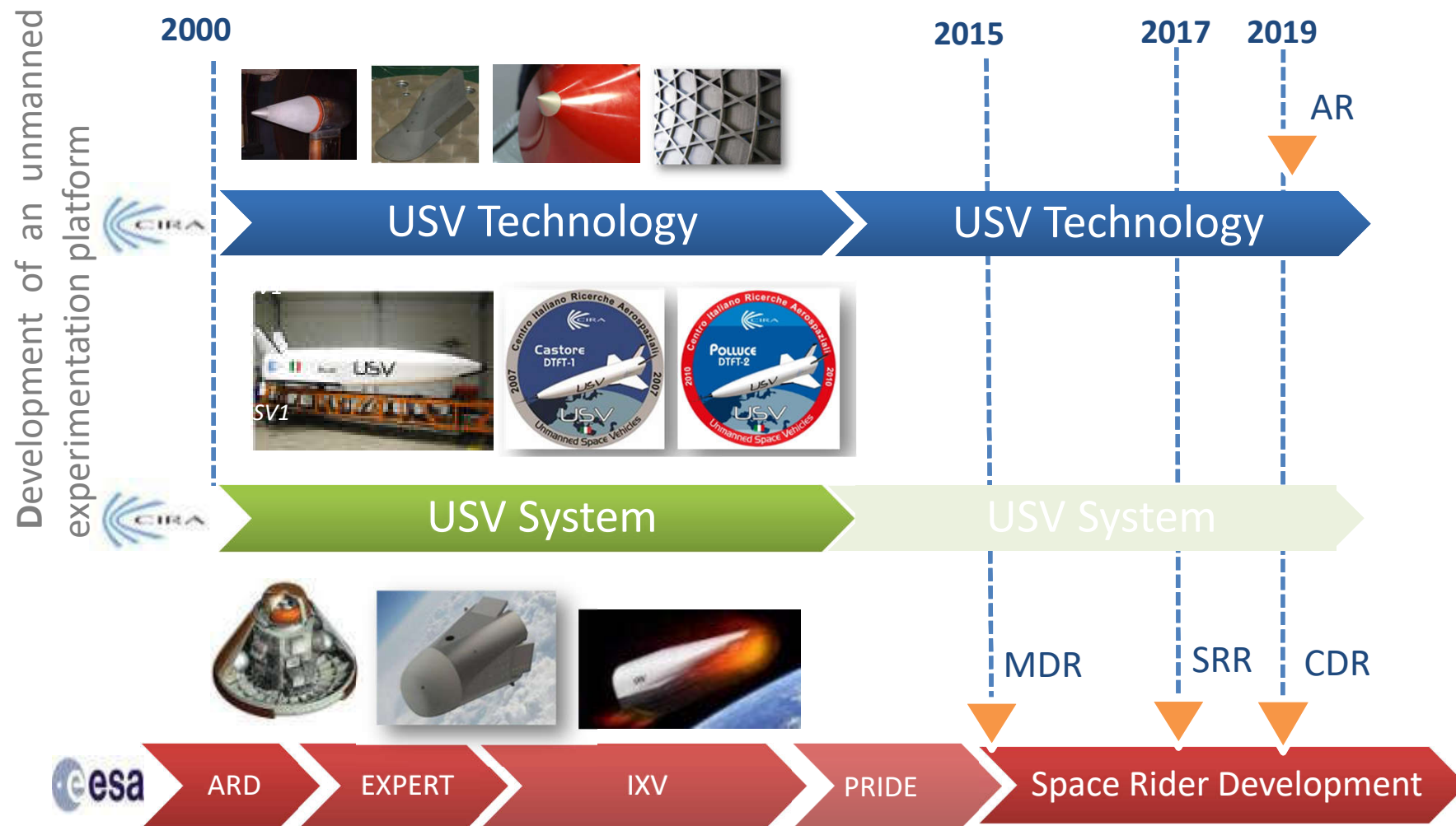


Plasma Wind Tunnel

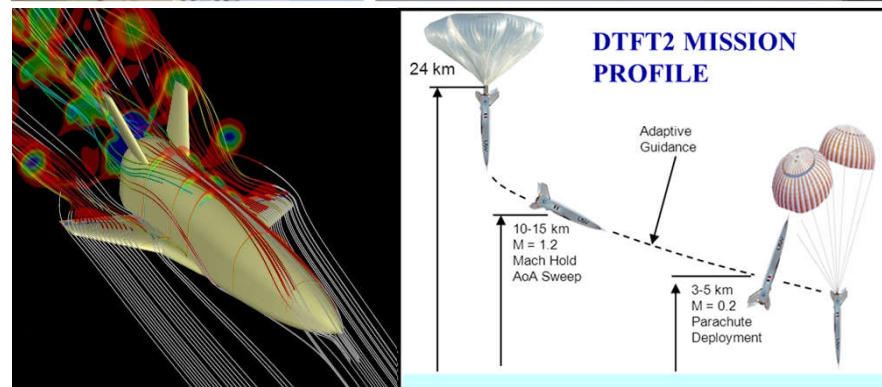


- ┌ Qualification capabilities ESA ECSS E-10-03-A “Space Engineering – Testing” & MIL-STD 810F for:
 - Physical properties measurements
 - Acceleration test
 - Combined vibration, humidity, temperature and altitude test
 - Environmental stress screening
 - Thermal shock test
 - Thermal vacuum test
 - Pyroshock test
- ┌ Equipment under test (EUT) of nominal dimensions 400x400x400 mm and 20 kg weight
- ┌ Equipped with flanges and standard MIL connectors to link the EUT with an EGSE for the transmission of excitation and monitoring signals to verify the EUT functionalities during the test

CIRA Unmanned Space Vehicle : more than 15 years of Italian research on re-entry technologies



- ❑ **Objective:** development of an unmanned experimentation platform.
- ❑ **Scope:**
 - Validation of key enabling technologies : aerodynamics, aerothermodynamics, material, structures, guidance navigation and control.
 - Demonstration of system capabilities to perform “glided” re-entry from sub-orbital or LEO conditions.
- ❑ **1st Drop Transonic Flight Test: 02/2007**
- ❑ **2nd Drop Transonic Flight Test: 04/2010**





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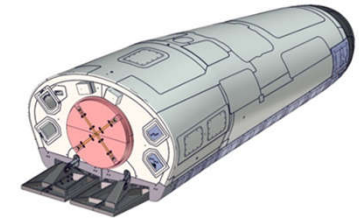


European Space Agency

IXV MISSION

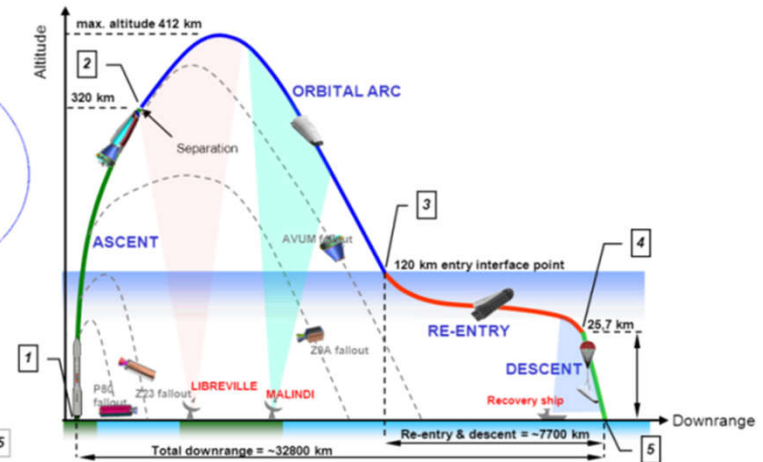
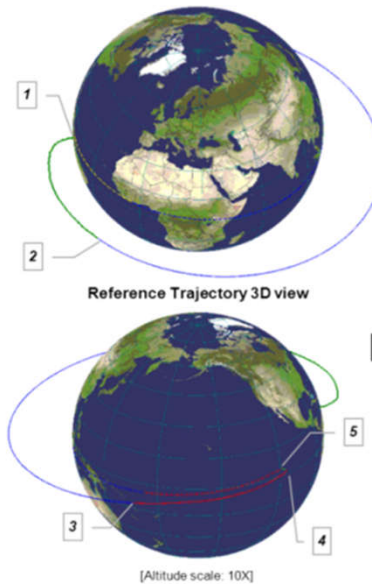
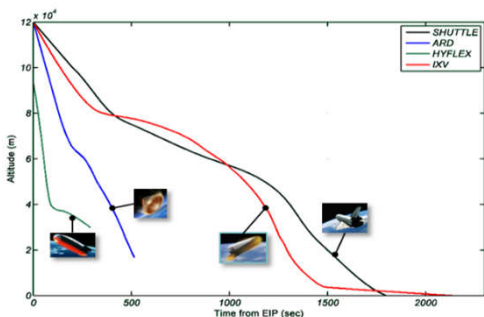
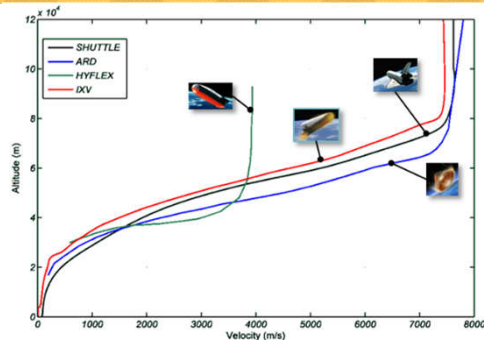
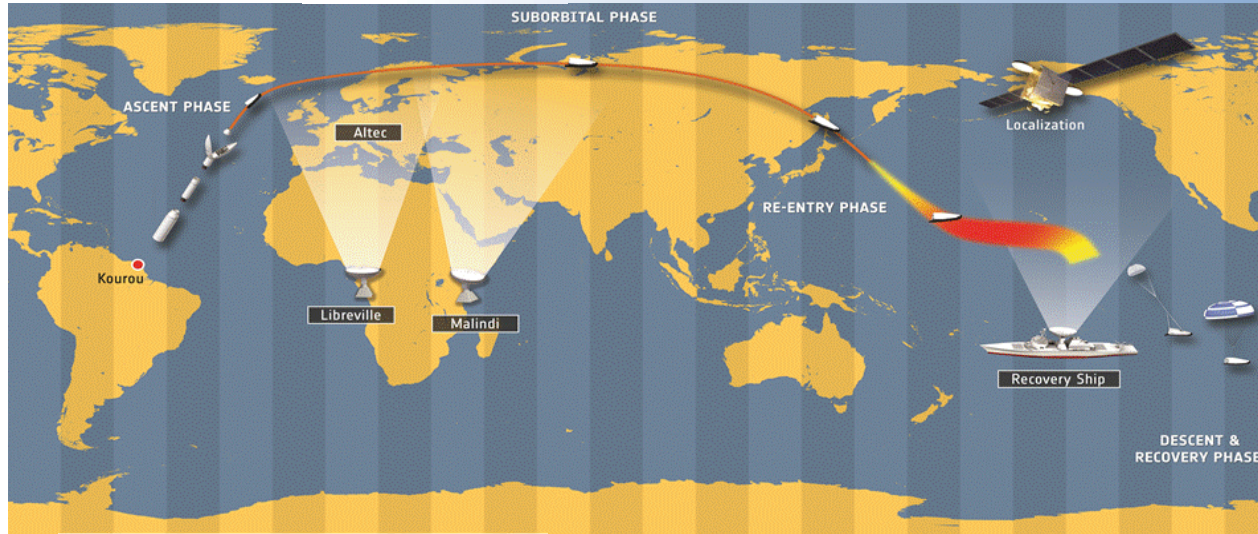
System Demonstration

First lifting-body system flying a fully representative return mission from LEO world-wide



Technologies In-flight Verification

- Advanced thermal protections and hot structures (with ceramics and ablatives)
- Advanced guidance navigation and control techniques (with thrusters and aero-flaps)
- Advanced Aerothermodynamics investigation techniques (with ≥ 300 integrated sensors)



Reference Timeline

| | | | |
|------------------|--------------|--------------------|----------|
| 1 - Lift off | T = 0 [s] | → Ascent segment | 966 [s] |
| 2 - Separation | T = 966 [s] | → Orbital segment | 2891 [s] |
| 3 - Entry gate | T = 3857 [s] | → Re-entry segment | 1323 [s] |
| 4 - Descent gate | T = 5180 [s] | → Descent segment | 881 [s] |
| 5 - Splashdown | T = 6061 [s] | | |

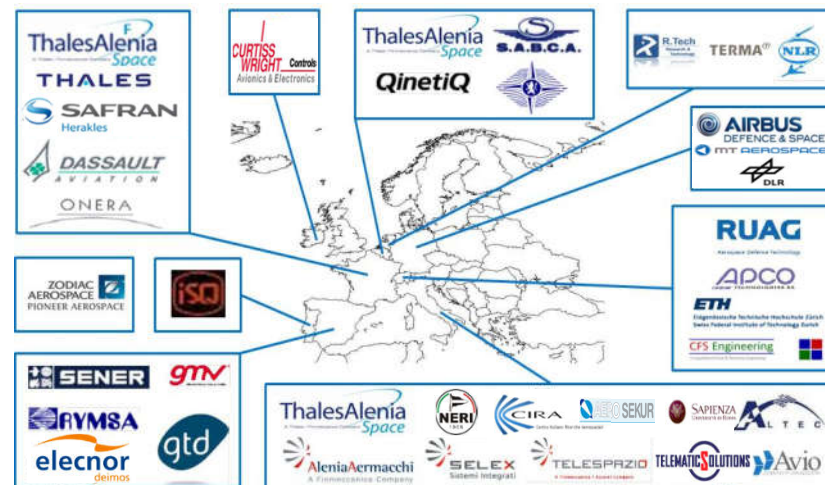
The IXV mission was successfully performed on the **11th of February 2015**, with all flight hardware and all flight data successfully recovered, through flight segment telemetry transmission and ground segment acquisition, and on-board recording, with the confirmation that the flight data is complete and consistent among the various sources.

The IXV system, and all associated technologies, have successfully performed the whole flight program in line with the commanded maneuvers and trajectory predictions, performing an overall flight of approximately 25.000 km including 8.000 km in hot atmospheric re-entry environment with automatic guidance, starting from an orbital velocity of ~ 7.5 km/sec (Mach=27), concluding with precision landing.

100% of the IXV mission, system and technologies objectives have been successfully achieved.



- **ENGINEERING ACTIVITIES**
 - ✓ aerodynamics
 - ✓ aerothermodynamics,
 - ✓ technologies demonstration in flight
 - ✓ thermal protection systems qualification
- CIRA specialists were part of the ESA team during the **IXV DEVELOPMENT, LAUNCH AND MISSION EXECUTION.**
- **DESIGN AND EXECUTION OF THE DROP TEST** performed from a helicopter of an IXV prototype scale 1:1; the goal was to test parachute and buoyancy safety system.
- **IXV POST FLIGHT ANALYSIS**





IXV EXHIBITION IN CASERTA ROYAL PALACE, JUNE-JULY 2015

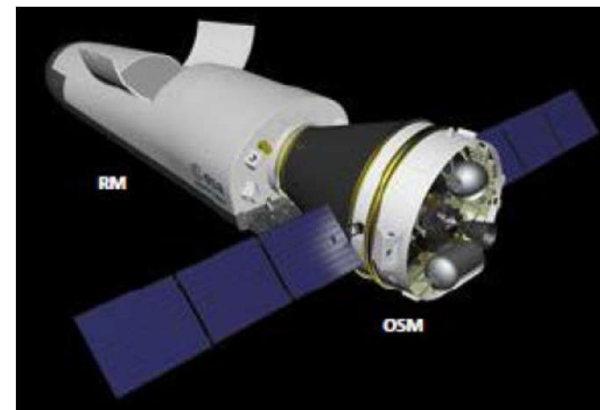
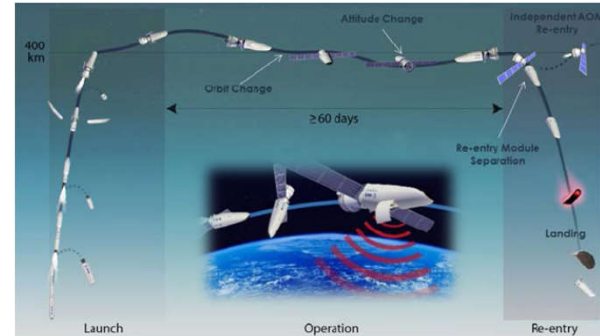


Goals:

- To develop an **affordable and sustainable** reusable European space transportation system:
 - to enable **routine access to and return from space**
 - to provide a **standardized platform for Payloads** for multiple space application in a multitude of orbits
- To focus on the **demonstration of a recurring service.**

Main Mission scenario:

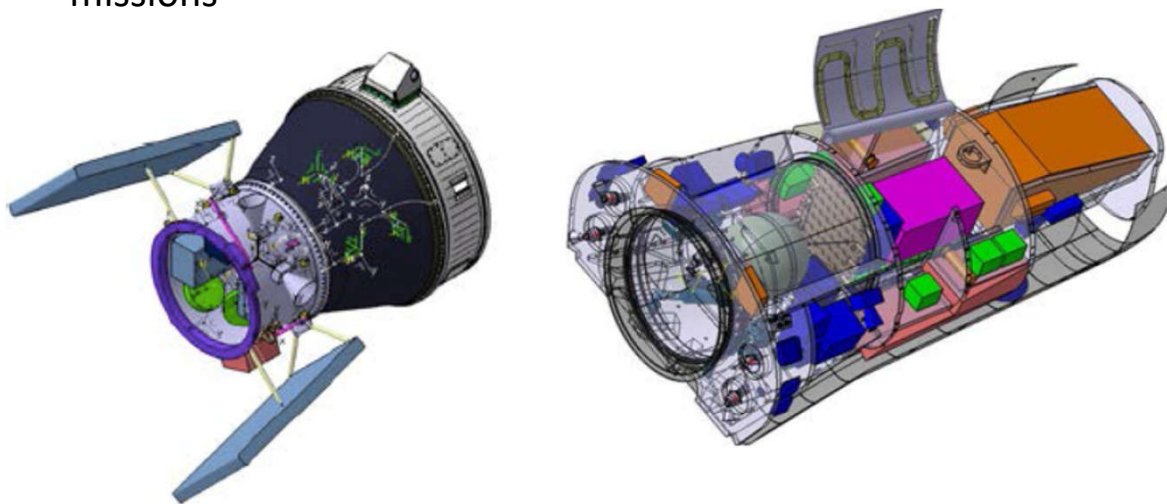
- **Free Flyer:** Microgravity Lab
- **In Orbit Demonstration:**
 - Exploration (e.g. robotics)
 - Earth observation (e.g. instrumentation);
 - Others (e.g. Earth science, telecommunication).
- **Surveillance applications** (e.g. earth monitoring, satellite inspection)
- Phase-B1 completed in December 2017
- Activities for Phase-B2/C started on January 2018:
System PDR in Q4 2018





MAIN SYSTEM FEATURES

- Launched with VEGA C and injected in LEO. Reference orbit for max payload: (400 km – 5deg).
- Payload mass larger than 650 kg for the reference orbit.
- Payload volume larger than 1.0 m³.
- In-orbit operational capability of at least 2 months.
- Precision ground landing allowing fast payload recovery time.
- Main landing site on European territory.
- System reusability with minimum refurbishment for 6 missions



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Since 2000, in the framework of the national aerospace research program (PRORA-SHS) and within various other National and European programs, CIRA together with CNR-ISTEC have studied, developed, and tested monolithic UHTCs and, in cooperation with CSM, UHTC coatings on different high temperature structural materials.

Small winglets and nose made in UHTC (EXPERT and SHARK project) or UHTC coated (SCRAMSPACE project) were designed, manufactured and installed on rockets or re-entry vehicles for in-flight qualification. Unfortunately, only the SHARK nose tip experienced the flight environment.



ASA
WLE Demonstrator made of CMC coated with UHTC



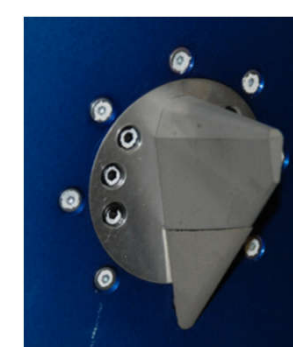
SHS
Nose Cap Demonstrator:
the tip is made of massive UHTC



EXPERT
Structural aerodynamic
profile made of massive
UHTC ; UHTC-METAL I/F



SHARK
Structural aerodynamic
profile made of massive UHTC



SCRAMSPACE
Structural aerodynamic
profile made of metal UHTC
coated and massive UHTC

- Massive UHTCs have proven extreme thermal resistance and chemical stability but the low toughness and low machinability make very hard to realize large and complex components.
- UHTC coating can improve the performances of some refractory metal or CMC that can withstand very high temperature, but that suffer erosion because oxidation.

Combination of refractory metallic substrate and UHTC coating able to withstand:

- up to 1700°C
- for more than 7 minutes
- for more than one test
- without erosion

The tests have also shown that when the coating exceeded its working temperature, the failure stays localized in the overheated region, without propagations.

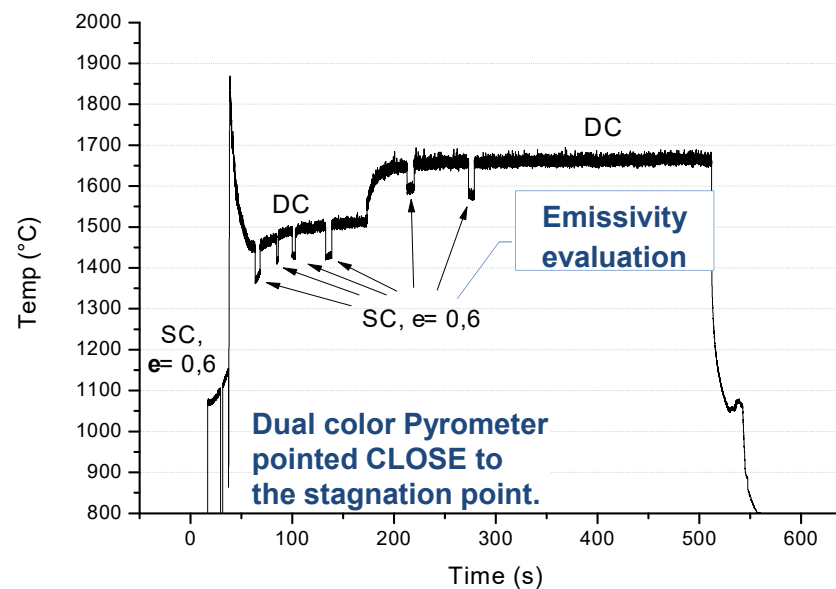


UNTESTED

TESTED

UNCOATED

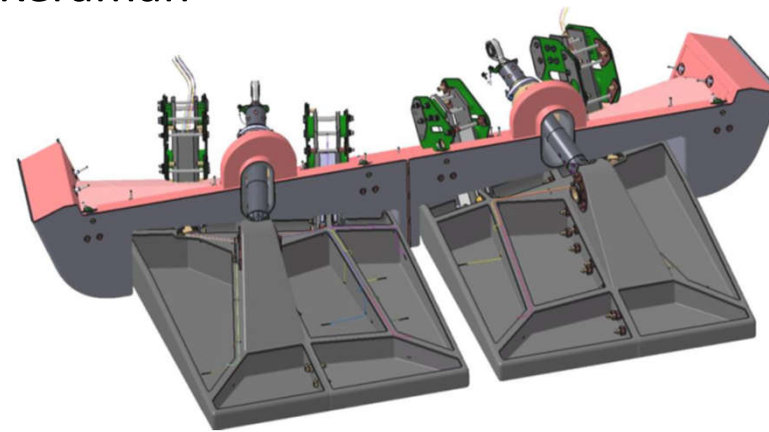
The samples survived temperature exceeding 1700°C for several minutes with no erosion.



IXV Body Flap Assembly by MT Aerospace



Keraman®



PRIDE Control Surface Assembly by ?

Italian Research Consortium



Since 2016, CIRA is leading a consortium of Italian excellence in the ceramic materials sector for the manufacture of C/SiC components with low cost techniques based on the Pyrolysis + LSI + Coating of SiC processes.



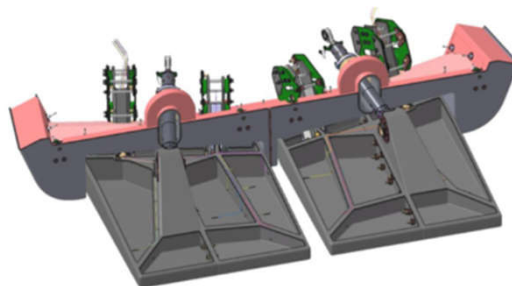
Pyrolyzed CFRP



CMC



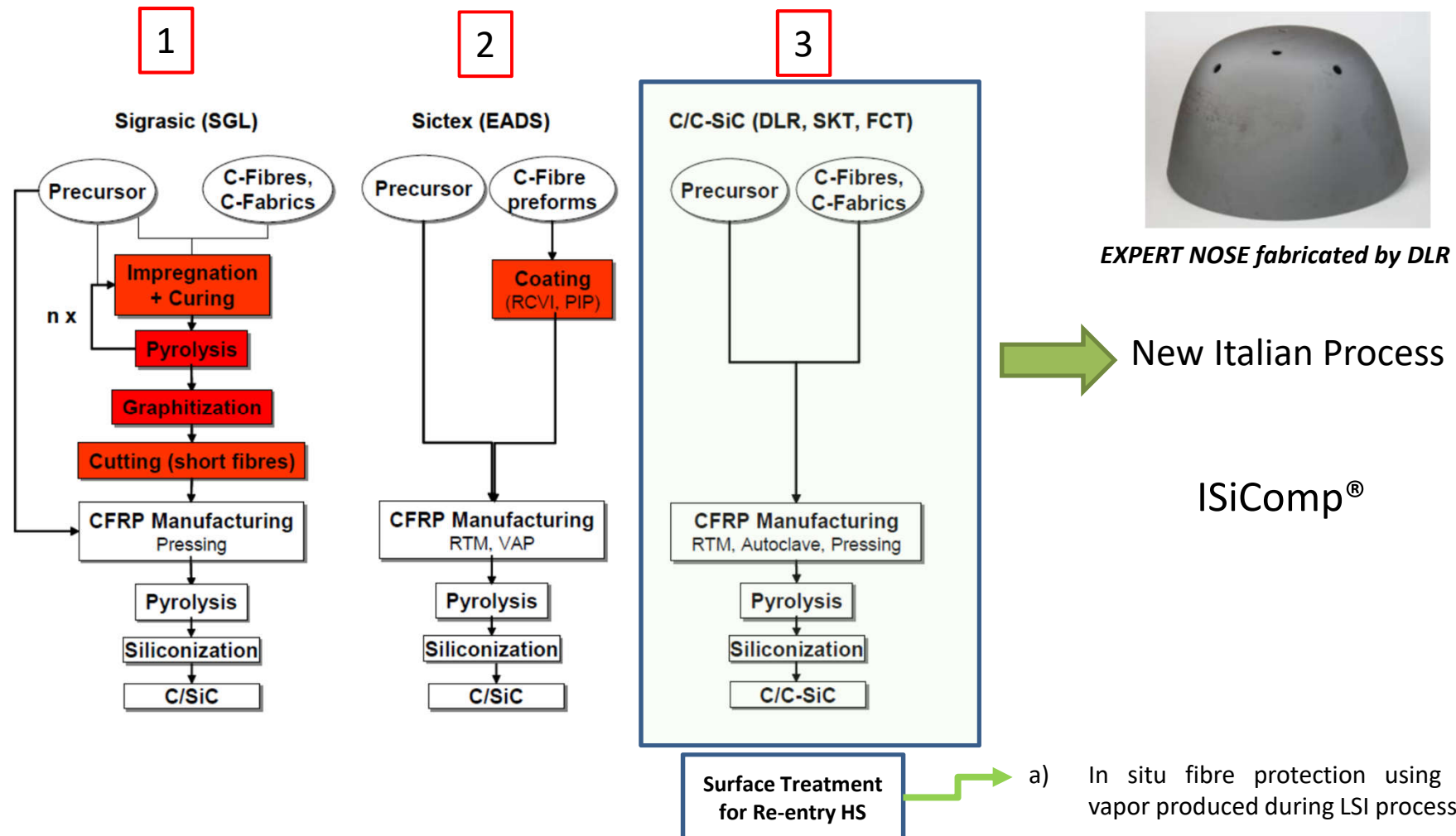
*Pyrolysed and siliconized phenolic base CFRP samples
(CIRA / Petroceramics)*



PETROCERAMICS



Liquid Silicon Infiltration (LSI) / Melt Infiltration (MI) Manufacturing Processes are based on 3 different methods to assure fibre protection and weak fibre/matrix bonding



- **MATERIAL SELECTION:**

- Phenolic prepreg fabric manufactured in Italy coupled with different type of fibers (following a trade off)

- **CFRP:**

- different autoclave routes to set up the optimal process parameters (pressure, lay up, thermal cycles) vs properties and geometrical constraints

- **PYROLYSIS:**

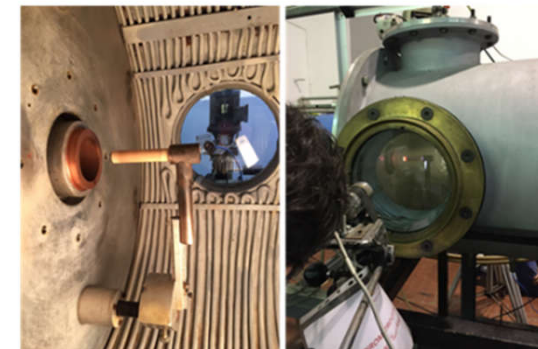
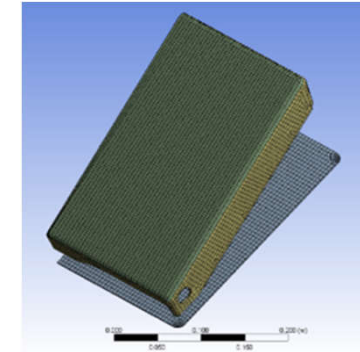
- test of different pyrolysis cycles to set up the optimal process parameters (time, temperatures)

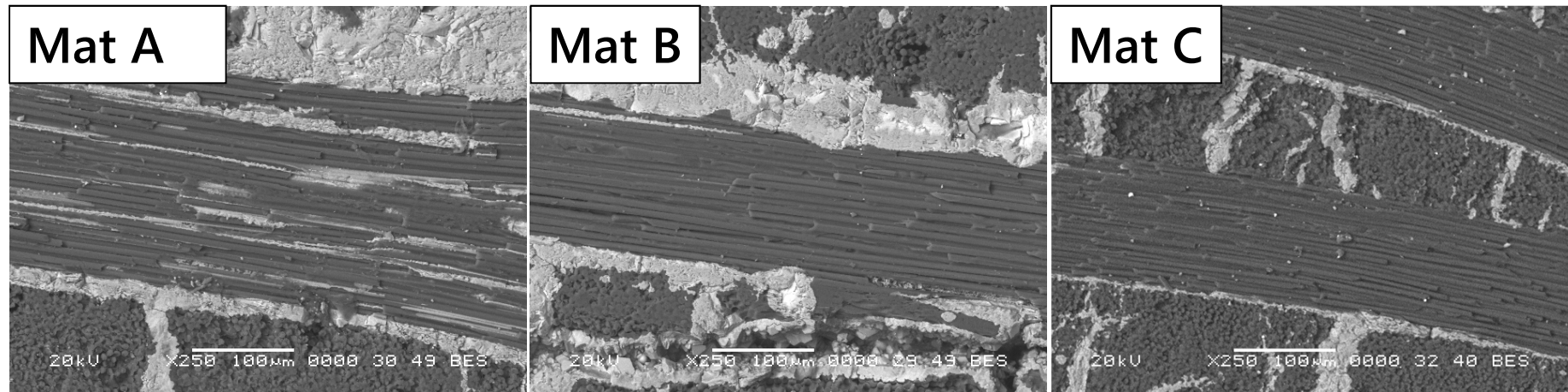
- **SILICONIZATION:**

- Si infiltration to set up set up the optimal process parameters (time, temperatures)

- **SEM, THERMAL AND MECHANICAL CHARACTERIZATION**

- **THERMO-MECHANICAL MODEL SET-UP AND VALIDATION**





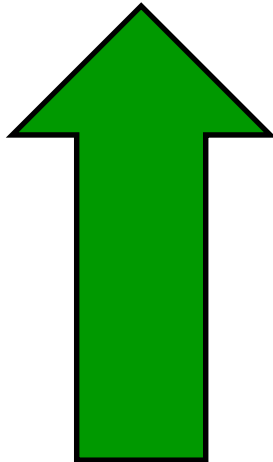
bundles silicon infiltration

Slight bundles silicon infiltration

No bundles silicon infiltration
Low overall silicon infiltration

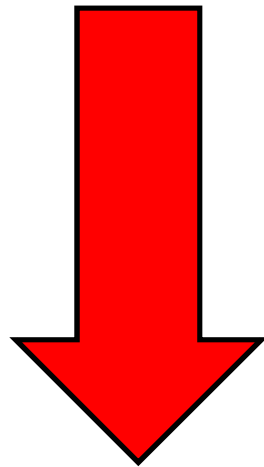
Mechanical properties increasing

Composite features vs mechanical properties



High fracture toughness

- No bundles silicon infiltration
- Fibers and bundles pullout
- Quite low fiber-matrix adhesion



Low fracture toughness (brittle behaviour)

- Bundles silicon infiltration
- Too high fiber-matrix adhesion



| PROPERTY of the selected material (Resin/Fibers) | VALUE |
|--|---------|
| E-Modulus | 56 Gpa |
| Tensile strength | 150 Mpa |
| Flexural strength | 200 MPa |

Table 5.4 Material properties of fabric and short fiber reinforced C/C-SiC and C/SiC material variants, obtained by LSI (DLR, SGL, SKT).

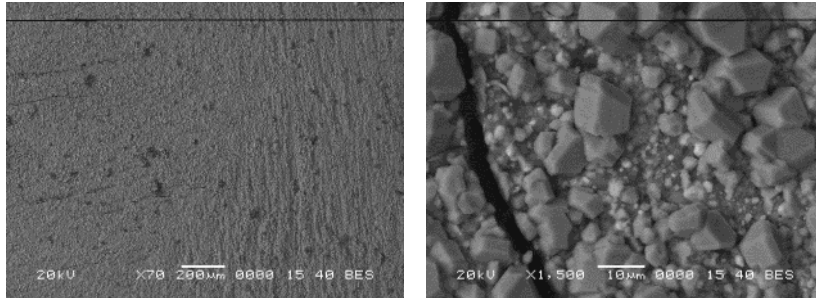
| Material properties | Unit | C/C-SiC | |
|-----------------------------------|----------------------------------|----------------------|---------------------|
| | | XB | XT |
| Manufacturer | – | DLR | DLR |
| Fiber reinforcement | – | Fabric | Fabric |
| Density | gcm ⁻³ | 1.9 | 1.92 |
| Open porosity | % | 3.5 | 3.7 |
| Young's modulus ^a | GPa | 60 | 100 |
| Flexural strength | MPa | 160 | 300 |
| Tensile strength | MPa | 80 | 190 |
| Strain to failure | % | 0.15 | 0.35 |
| Thermal conductivity ^a | W/mK | 18.5/17 | 22.6/20.8 |
| | ⊥ | 9.0/7.5 | 10.3/8.8 |
| Specific heat (25 °C) | J kgK ⁻¹ | 750 | 690 |
| SiC content | vol.-% | 21.2 | 19.8 |
| Si content | vol.-% | 5.4 | 4.1 |
| C content | vol.-% | 69.9 | 72.4 |
| CTE | 10 ⁻⁴ K ⁻¹ | -1/2.5 ^d | -1/2.2 ^d |
| | ⊥ | 2.5/6.5 ^d | 2.5/7 ^d |
| Ref. Temp. = 25 °C | | | |

|| and ⊥ = fiber orientation.
a 0–300 °C/300–1200 °C.
b 20/1200 °C.
c 25–800 °C.
d 100/1500 °C.
e 25/1400 °C.
f 50 °C.
g 200/1600 °C.

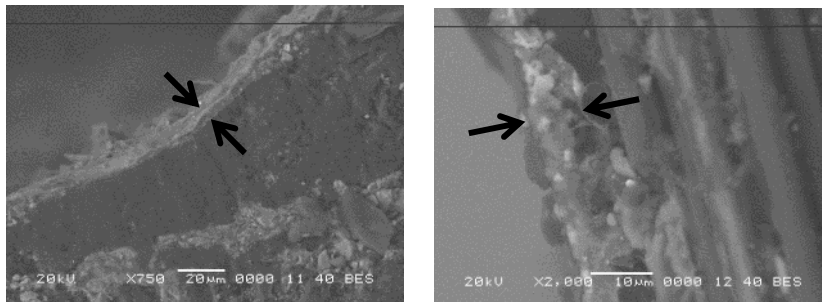


Expert Nose
manufactured using C/C-SiC XB material

SEM- Surface



SEM - Cross section

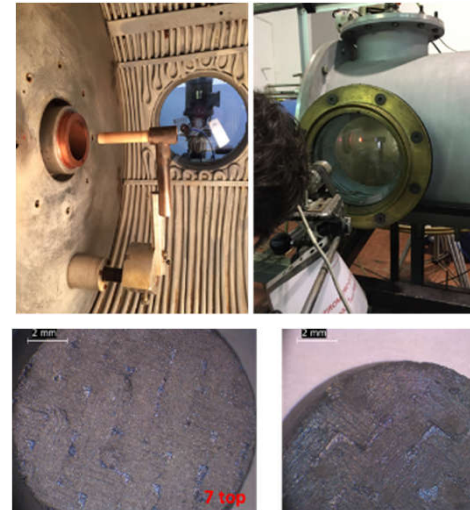


- The coating is made by a reaction process and not a deposition one
- Coating can be easily reapplied after use (reusability).

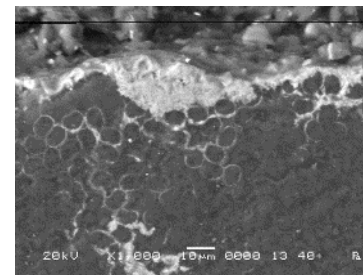
PLASMA ARC-JET TESTS

No active oxidation under relevant environmental testing carried out in plasma arc-jet facilities CIRA-GHIBLI

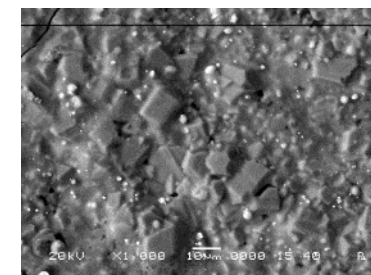
- Tmax = 1600°C
- P02= 2500 Pa
- Exp. time 600 s



SEM - Cross section



SEM- Surface



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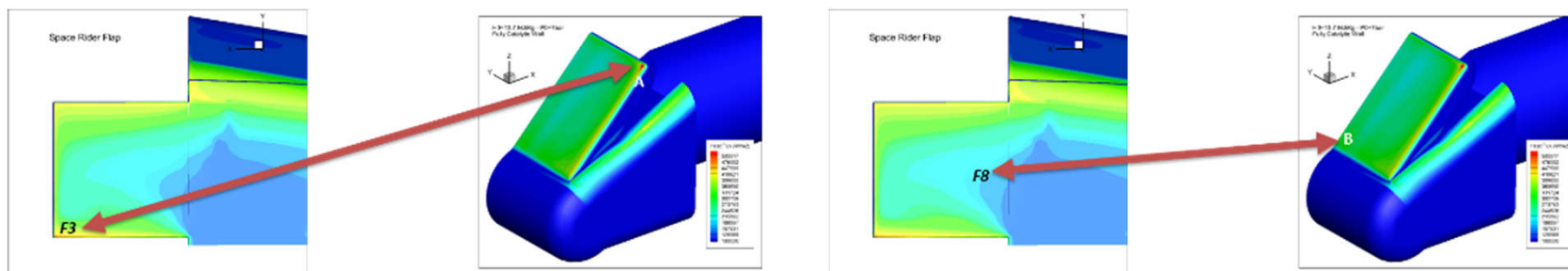
The goal of this test is to assess the behavior of the CMC technological demonstrator developed in the frame of Pro.R.A. funded SHS program in representative conditions of Space Rider atmospheric re-entry.

The test article has the same geometry of the EXPERT flap. This choice was driven from a twofold benefit:

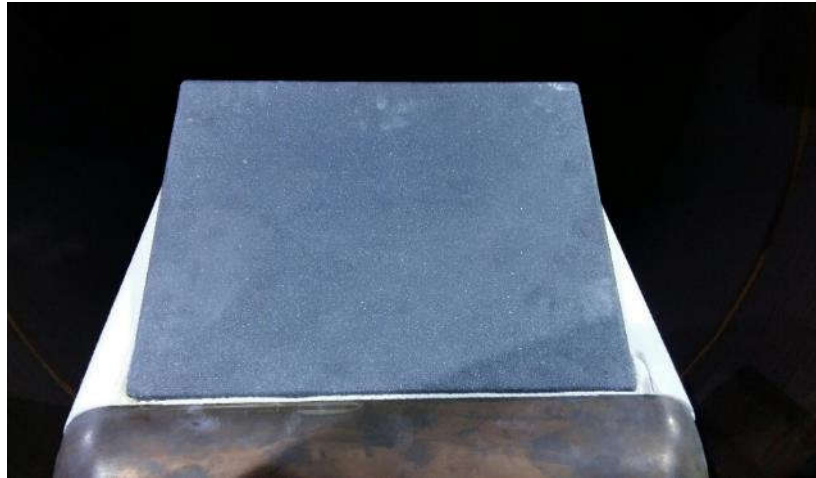
- ✓ from one side the availability of the same test holder;
- ✓ from the other side to have a direct comparison in terms of aerothermal loads with a well assessed CMC technology, provided by MT-A, already tested in PWT environment.



Maximize the similarity with EXPERT test in order to have a direct benchmark for SHS CMC demonstrator test;
 Stress the demonstrator with thermal conditions representative of the ones expected for Space Rider re-entry mission.



| <i>SR Trajectory</i> | <i>SR Ref Point</i> | <i>Max heat flux</i> | <i>Max heat load</i> | <i>EXPERT Ref Point</i> | <i>EXPERT Heat Flux on ref</i> | <i>Equivalent test time</i> |
|----------------------|---------------------|----------------------|----------------------|-------------------------|--------------------------------|-----------------------------|
| <i>[-]</i> | <i>[-]</i> | <i>kW/m2</i> | <i>MJ/Kg</i> | <i>[-]</i> | <i>kW/m2</i> | <i>[s]</i> |
| Max Heat Flux | F3 | 514 | 264 | A | 500 | 530 |
| Max Heat Load | F3 | 343 | 353 | A | 500 | 700 |
| Max Heat Flux | F8 | 350 | 141 | B | 300 | 470 |
| Max Heat Load | F8 | 176 | 183 | B | 300 | 610 |



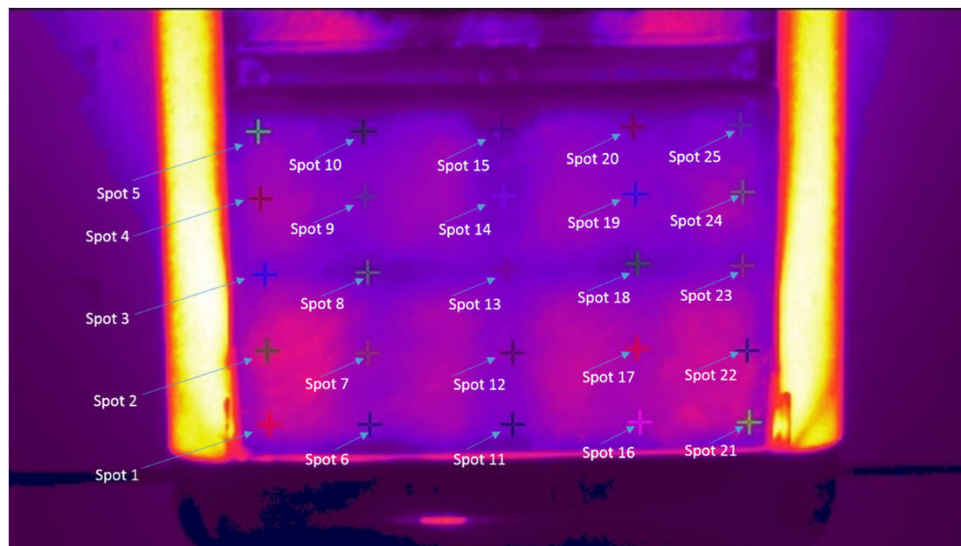
C/SiC 400mm x 300mm body flap demonstrator mounted on the Scirocco Model Holder



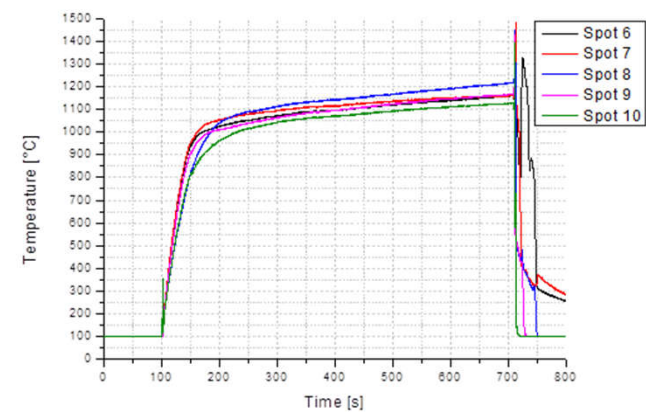
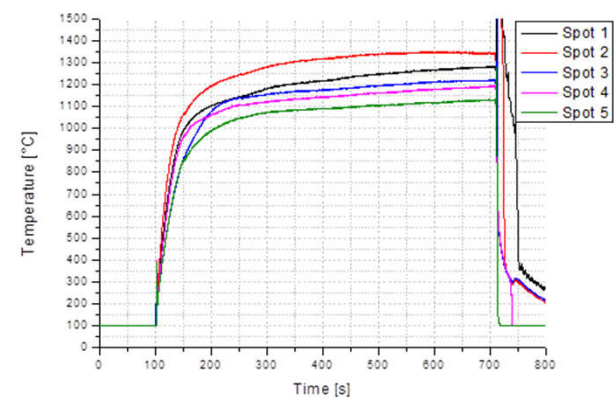
A first Plasma test in CIRA SCIROCCO facility has been performed on 18th of April on a 400 mm x 300mm reinforced flap demonstrator:

| | |
|--------------------------------|----------------|
| <i>Time</i> | <i>600 S</i> |
| <i>Experienced Temperature</i> | <i>1200 °C</i> |



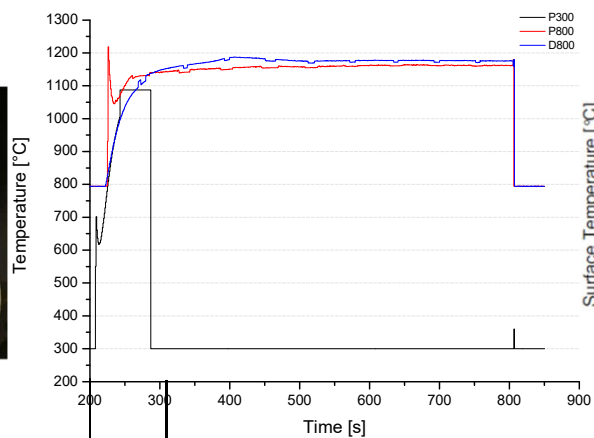
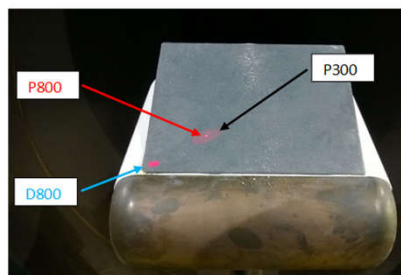


IR results require additional post processing



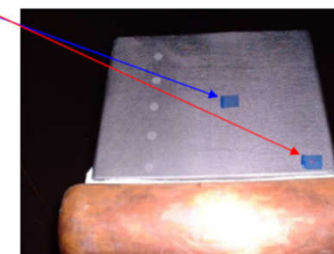
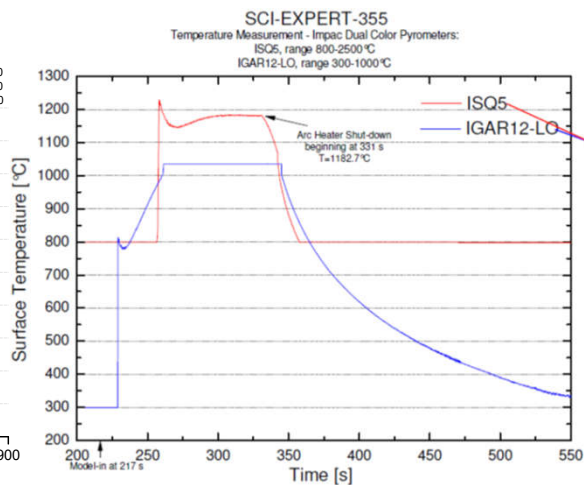
TEST SHS-SR CMC TECHNOLOGY DEMONSTRATOR, 2018

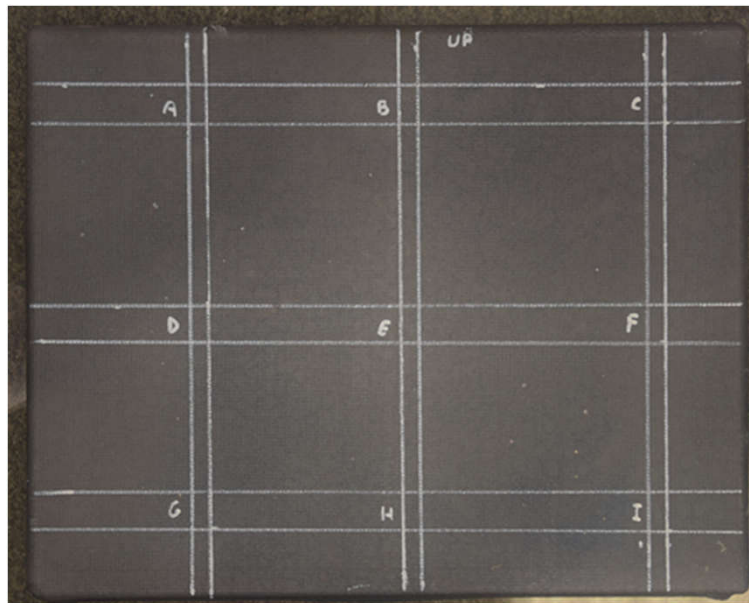
TEST EXPERT OPEN FLAP ASSEMBLY, 2011



110 s

EXPERT
OFA
TEST



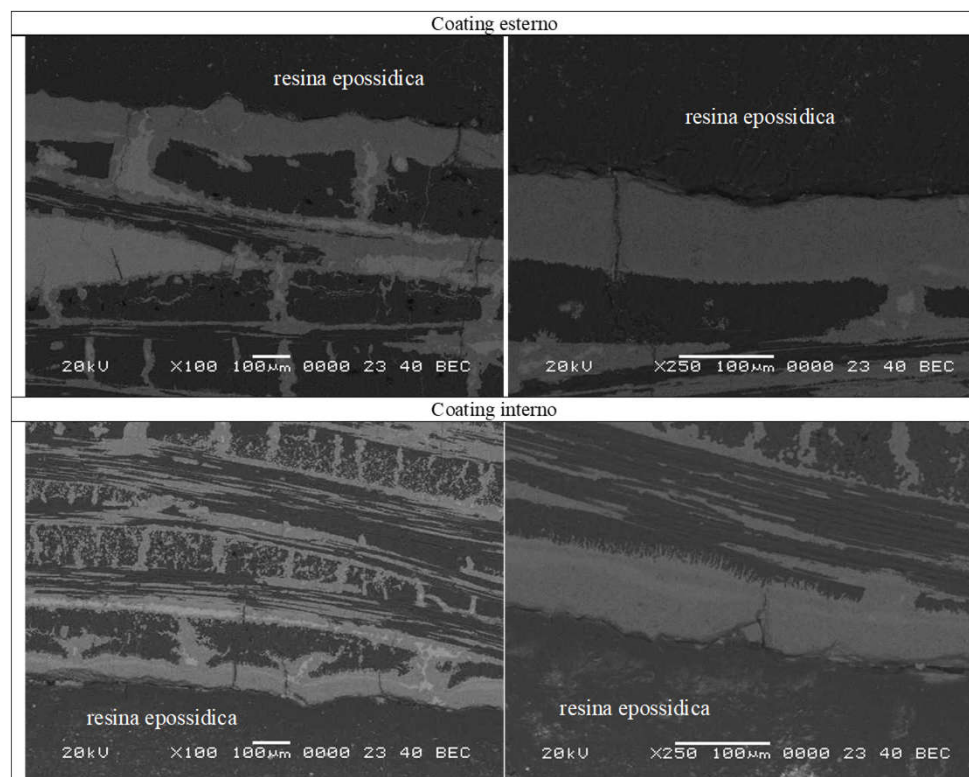


The specimens were incorporated in epoxy resin and subsequently polished with abrasive papers with decreasing FEPA granulometry (320, 500 and 1200).

The lapping and polishing process made it possible to observe the coating in section away from the area where the cut took place.

A sample was also taken from the inside, at an area with iridescent coloring. This specimen was observed on the surface as such, without performing polishing.

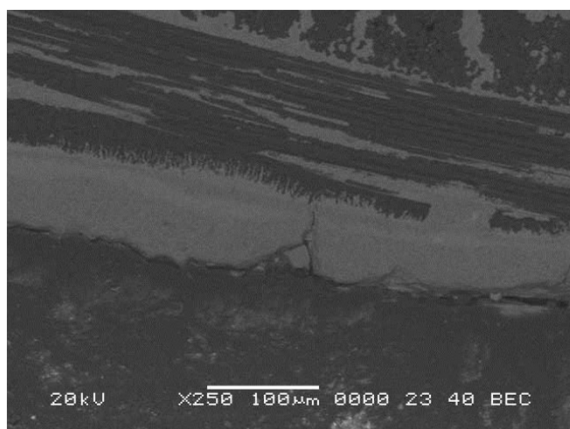
Specimen E



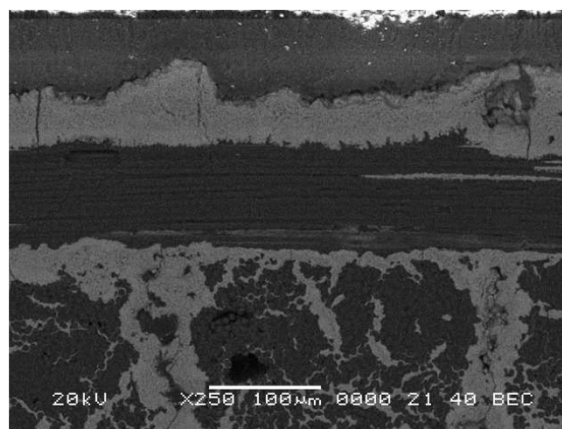
The coating on the external side appears compact and covering the entire surface. It has a high thickness, around 80-100µm. No signs of surface oxidation of the coating are observed.

Microcracks are observed which in some cases also involve part of the CMC. In correspondence of such cracks, however, no signs of oxidation of the fibers are observed.

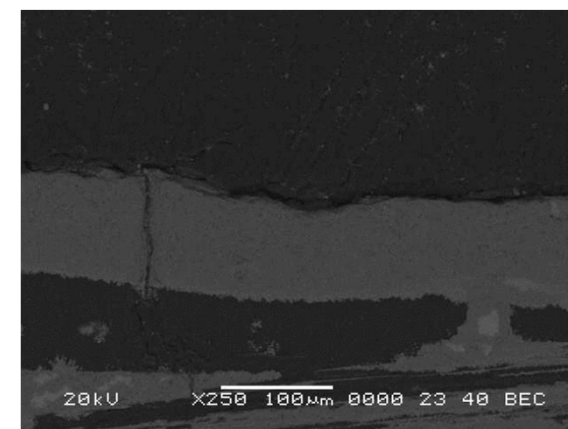
Inside



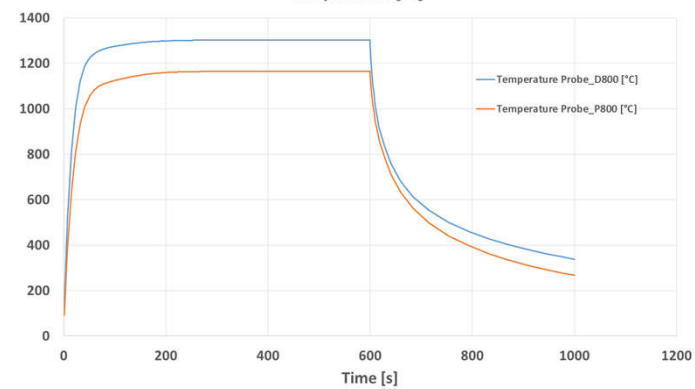
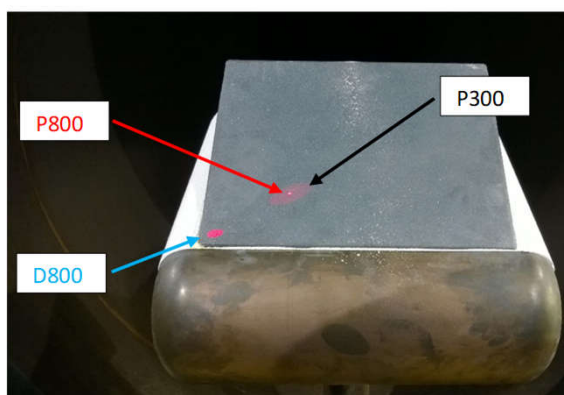
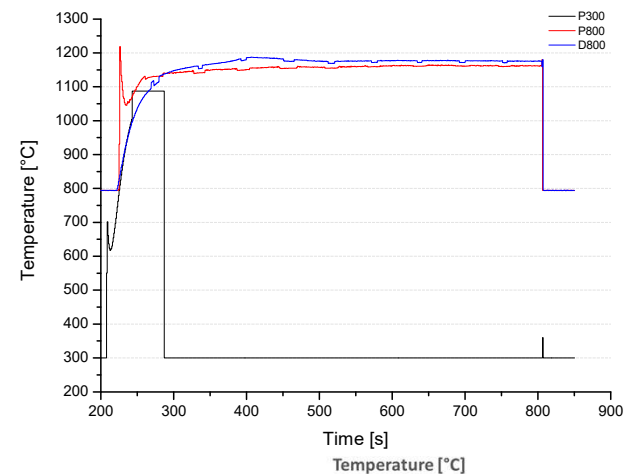
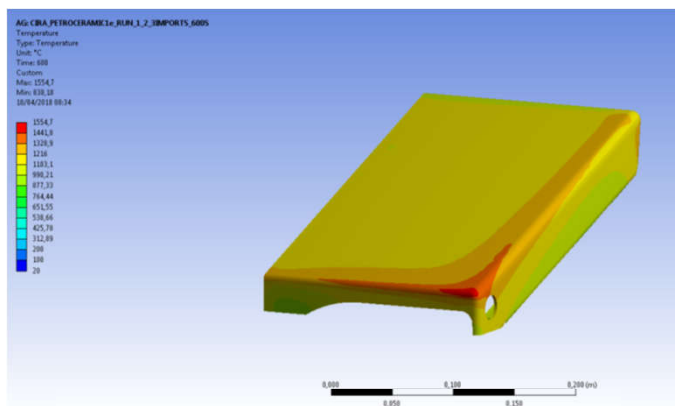
Witness coupon



Outside



The coating is very similar to that of the reference plate, both for thickness and for compactness and extent of cracking. No signs of deterioration of coating and CMC due to the test are observed.



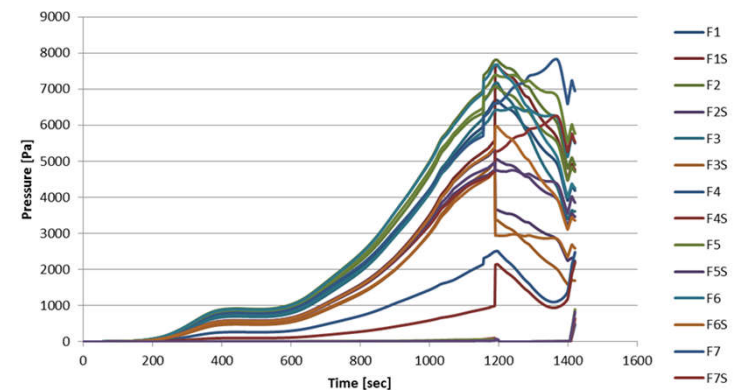
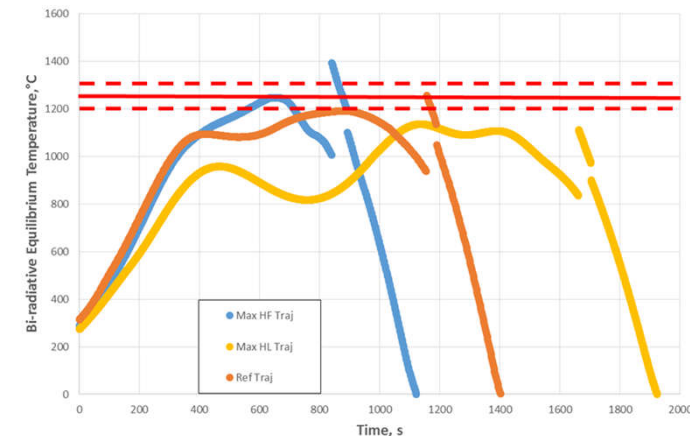
The temperature requirement has been defined by considering the bi-radiative equilibrium condition (i.e. body flap is assumed as a thin plate emitting in both windward and leeward surfaces with $\varepsilon=0.8$) on the GCP F3 along the reference trajectory.

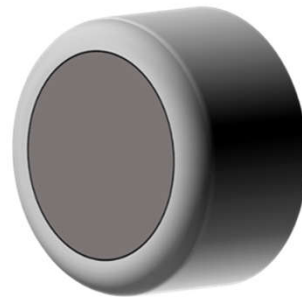
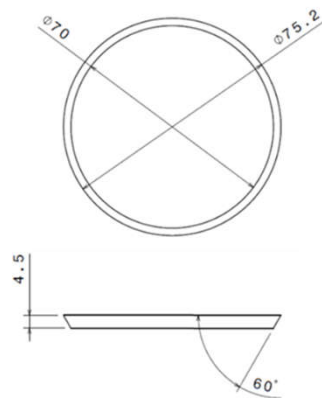
A constant temperature of $1250^{\circ}\text{C} \pm 50^{\circ}\text{C}$ shall be maintained at the center of the sample.

The duration of each cycle has been obtained by dividing the heat load obtained on the reference trajectory for the maximum heat flux (490 kW/m² due to laminar-turbulent transition) of the GCP F3:

$$\text{Duration} = 344 \text{ MJ/m}^2 / 490 \text{ kW/m}^2 = 690 \text{ s} \approx \mathbf{700 \text{ s}}$$

A constant wall pressure lower than 80 mbar shall be maintained throughout the test on the specimen wall in order to be compliant with pressure levels of flight conditions





The C/SiC materials samples are disks with 70 mm of exposed surface. They shall be slotted in the SCIROCCO Standard Model Holder.

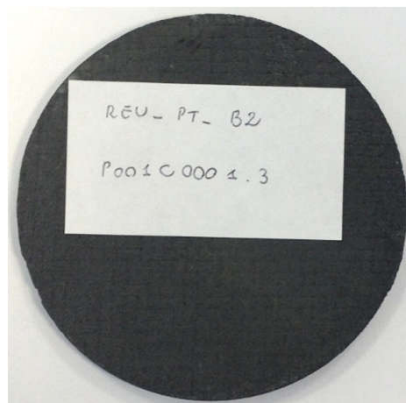
- Four samples are provided by two different process routes by application of the same process parameters in the frame of Batch#2 material characterization.
- For each process route the two samples will be used respectively as reference sample by evaluating bending strength and performing SEM analysis at the end of manufacturing process and as reusability test sample.
- The reusability sample will be exposed to aerothermal cyclic loads representatives of six re-entry flights. After tests the sample will be cut to obtain specimens for bending test strength and for SEM post-test analysis.

Short ID:113

Front



Back



Short ID:121

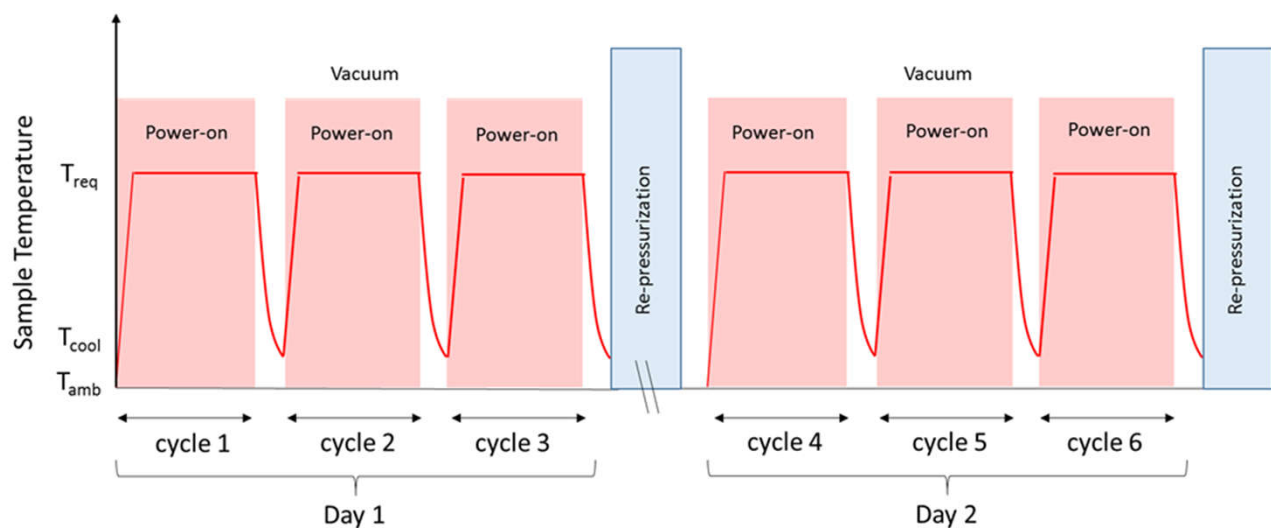
Front



Back

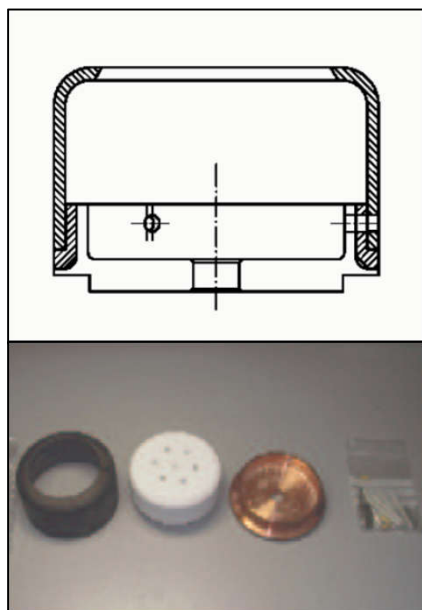


NOTE: Different sample colouring it's only a picture artifact



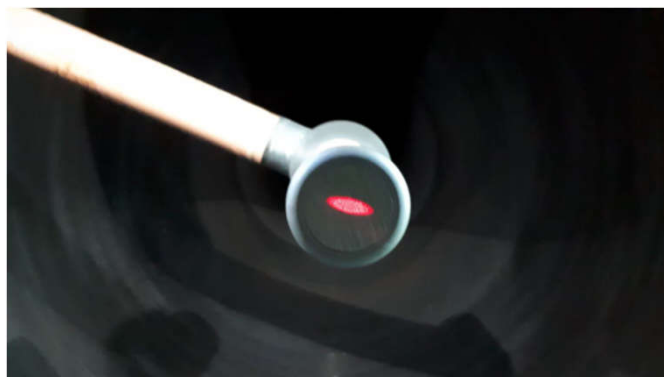
| Test Campaign | Sample ID | Type of Test |
|---------------|-----------|---------------------|
| 1 | 113 | PWT + Bending + SEM |
| 2 | 121 | PWT + Bending + SEM |

The model geometry consist in a flat faced cylinder, known as Standard Model Holder, not cooled, with the housing made of SiC and the inner made of bulk polycrystalline fibers, to be interfaced to an appropriate copper flange and then installed on the SCIROCCO cooled probe arm.

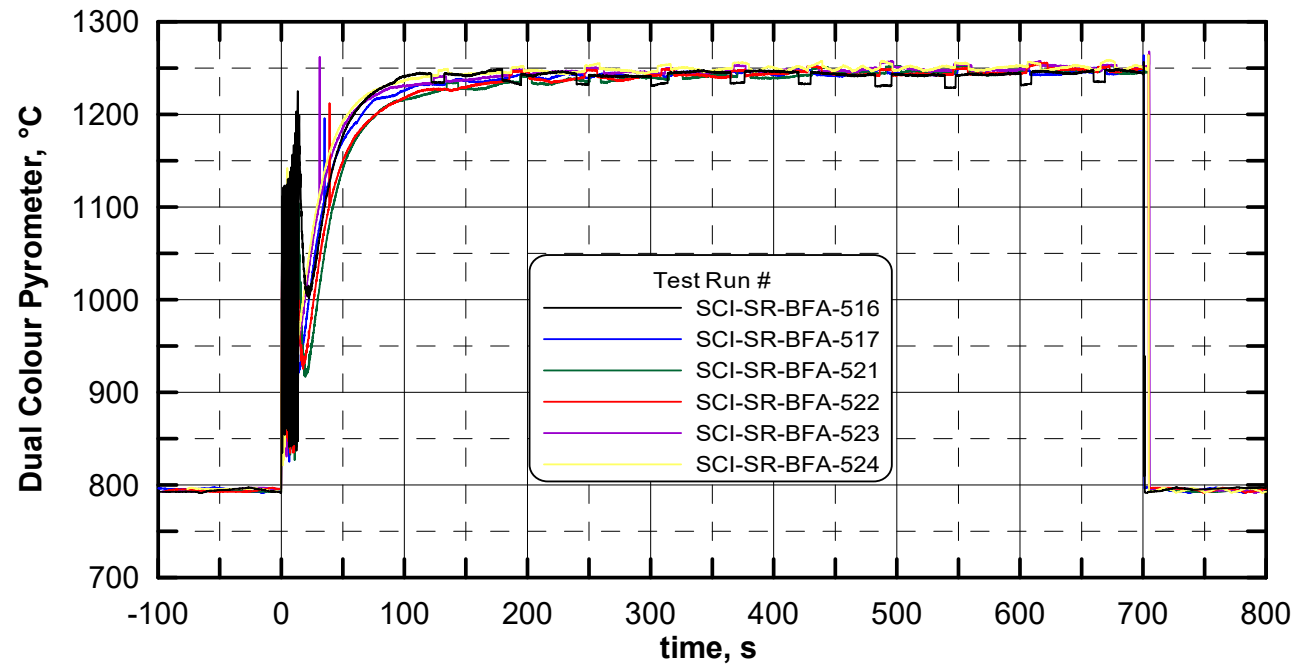


A dual color/single color 800-2500°C range is pointed on the center of the samples (left). Other two dual color/single color are pointed on the same position once the sample is out of the plasma jet to monitor the cooling phase, guaranteeing that between two cycles the sample temperature is below 400°C (right).

| Tag | Manufacturer | Model | Operative Mode | Range [°C] | Wavelength [μm] |
|------|--------------|------------|------------------|------------|-----------------|
| D800 | DIAS | DSRF 11N | Two/Single-Color | 800÷2500 | 0.7÷1.1 |
| P300 | IMPAC | IGAR 12-LO | Two/Single-Color | 300÷1000 | 1.52÷1.64 |
| P800 | IMPAC | ISQ5 | Two/Single-Color | 800÷2500 | 0.9÷1.05 |



SUMMARY



The sample has been exposed to the equivalent re-entry environment for an overall time of **4200 (1h 10')**

A confirmation of the temperature uniformity all over the sample surface has been obtained by Infrared Camera measurements.

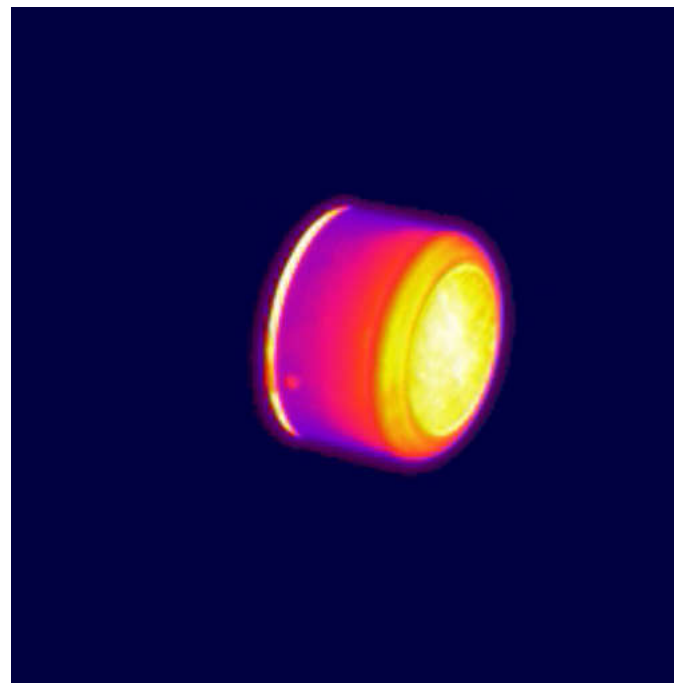


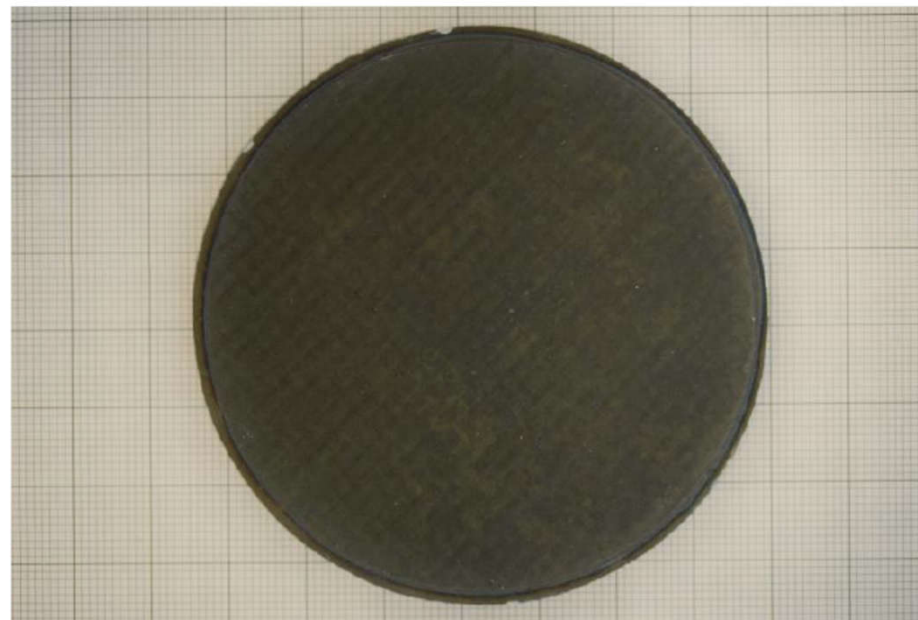
Image taken from Test Campaign #2 (raw data)

REFERENCE SAMPLES



Short ID:112

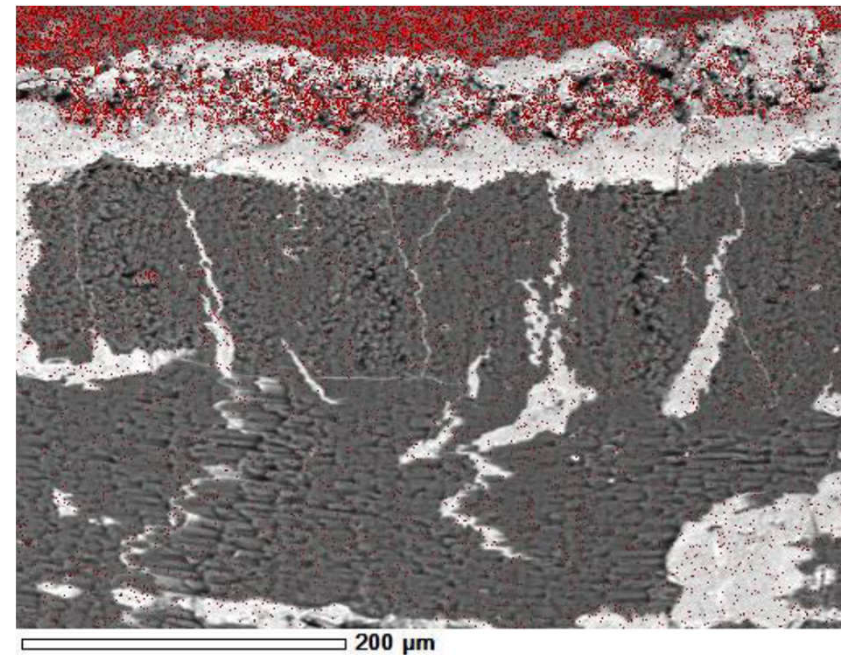
PWT TESTED SAMPLES

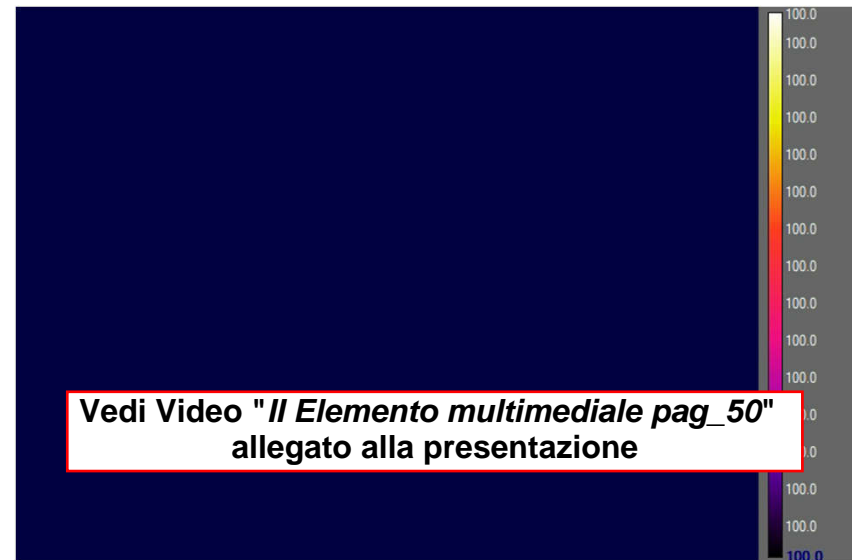


Short ID:113

Weight measurements were performed with ORMA BC 500 LCD (S011) (accuracy of 0.01g)
The samples were dried at 105 ° C for 2 hours before each weight measurement.
Mass loss below 0.3% has been measured.

The chemical map shows that oxidation affects only the external part of the coating. After the 6 cycles exposure an inner layer of compact coating consisting exclusively of SiC with a thickness of about $20\mu\text{m}$ can be observed. It is interesting to note that in the bulk of the composite no oxygen is found at SiC and free silicon.







Centro Italiano Ricerche Aerospaziali



END